

The importance of materials properties in high-temperature processes

Ken MILLS^{1,2}, Muxing GUO³

¹ Dept. Materials, Imperial College, London SW& 2AZ,

² University of Manchester

³ Dept. Metallurgy & Materials Eng. KU Leuven,

Physical properties & high-temperature processes

- Phys. Chem. Properties- useful in solving problems with process control and product quality.
- First law of high temperatures
- *“At high temperatures everything reacts with everything else”*
- Second Law:
- *“They react bloody quickly and situation worsens rapidly as the temperature increases”.*
- Many problems in high temp. processes- disaster never far away

Example- variable weld penetration

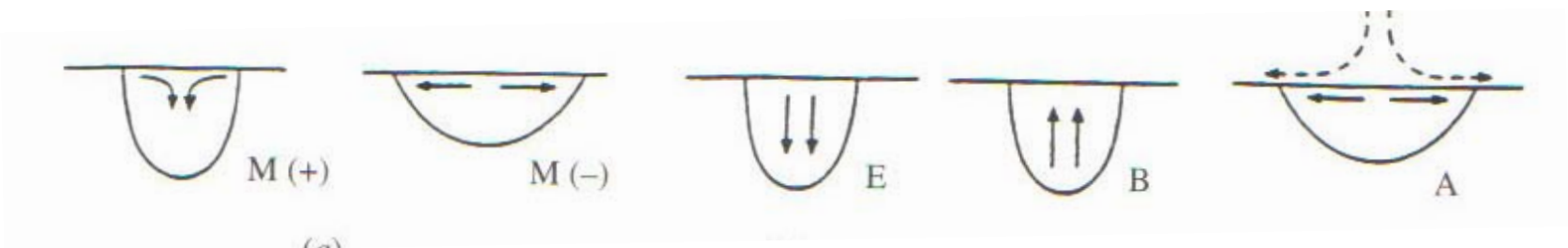
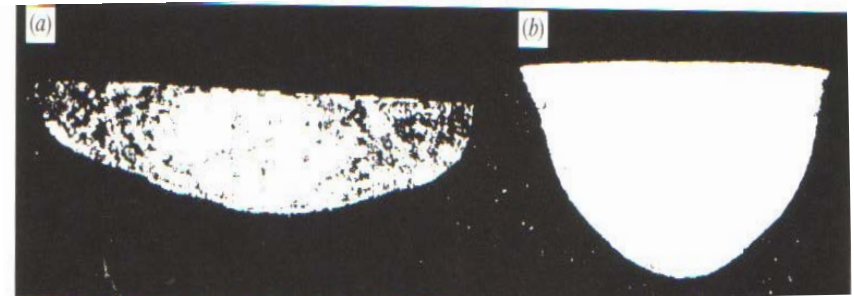
TIG/GTA welding-robotic process-many welds

-set up optimum welding-

Deep weld penetration

- Change steel- meets spec. -→shallow welds

- Forces acting in pool

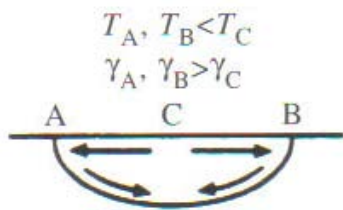
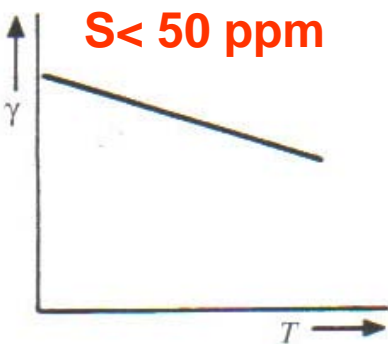


Effect of tiny differences in S

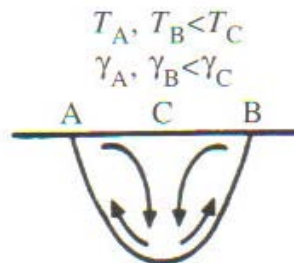
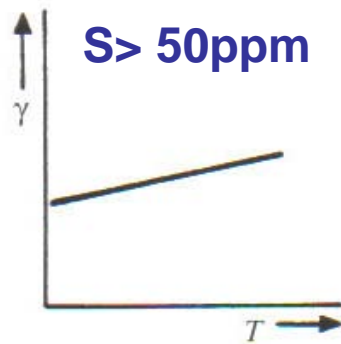
Surface tension >50steels

50ppm S → 25% ↓ in γ

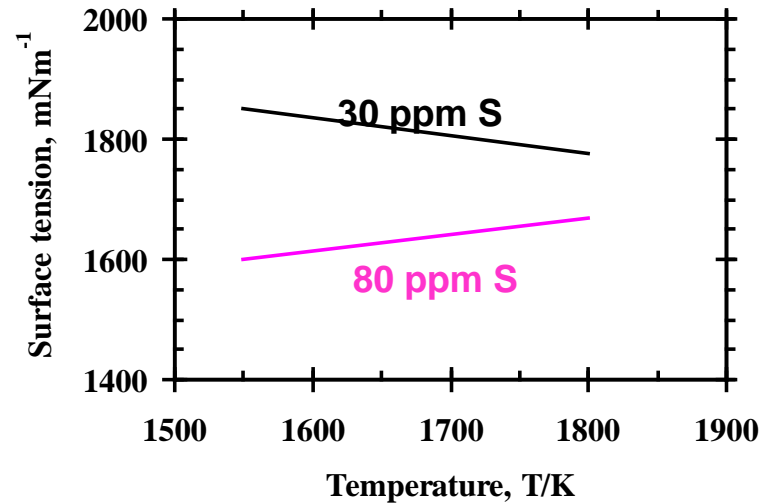
$d\gamma/dT \rightarrow -ve \text{ to } +ve$



(a)



(b)



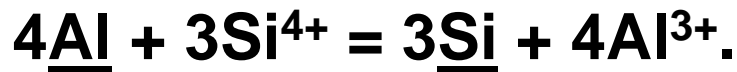
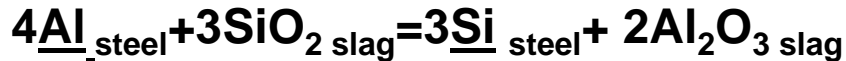
- Hot liquid → melt back
- <50 ppm S –flow outward–melt back–shallow weld
- >50 ppm S –flow inward & down → deep weld

Slag properties and structure

Problem caused by ppm differences in S

Math models improved → insights to mechanisms

-Slags- are ionic

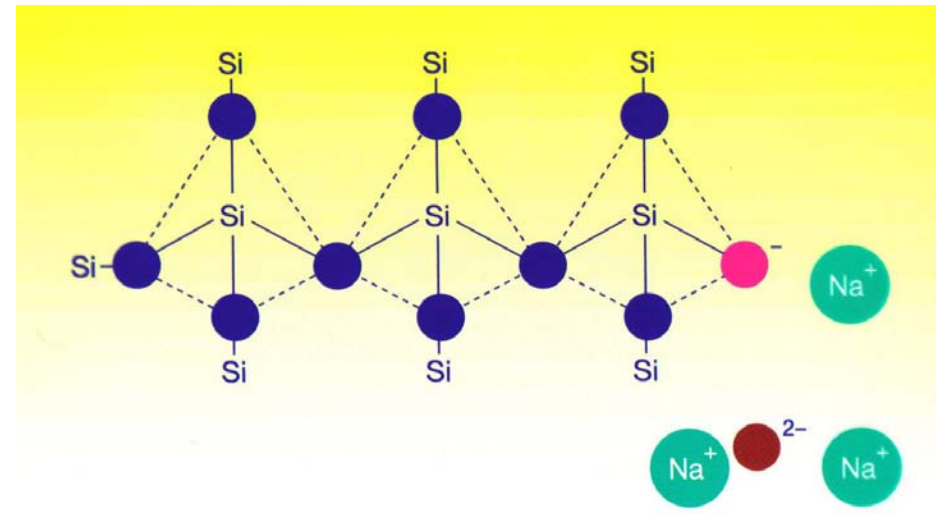


Slag props –depend on slag structure

Silicates- building block

Si- 4O tetrahedron with O joining 2 tetrahedra

Cations, Na⁺ - break bonds



BOs, NBOs and free O's

Alumino-silicates

Add Al_2O_3 -network breakers ↓

→ polymerisation ↑. $(4)\text{Al}$

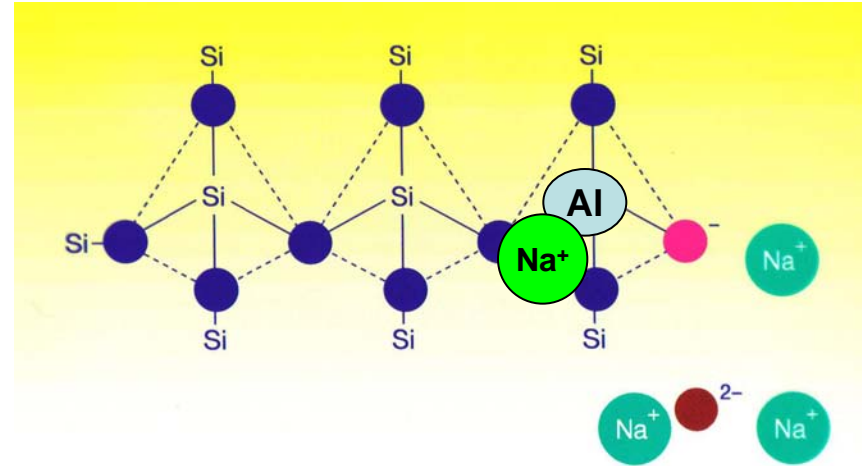
High Al_2O_3 → some $(5)\text{Al}$, $(6)\text{Al}$

$$\text{NBO/T} = 2 \left(\frac{\sum X_{\text{MO}} + \sum X_{\text{M}_2\text{O}} - X_{\text{Al}_2\text{O}_3}}{X_{\text{SiO}_2} + 2 X_{\text{Al}_2\text{O}_3}} \right)$$

$Q = (4 - \text{NBO/T})$ = measure of polymerisation

TiO_2 behaves like SiO_2 ?

Fe_2O_3 , Cr_2O_3 - behave as Al_2O_3 ?



Charge-balancing



Na^+ cannot act as network-breaker- polymerisation ↑

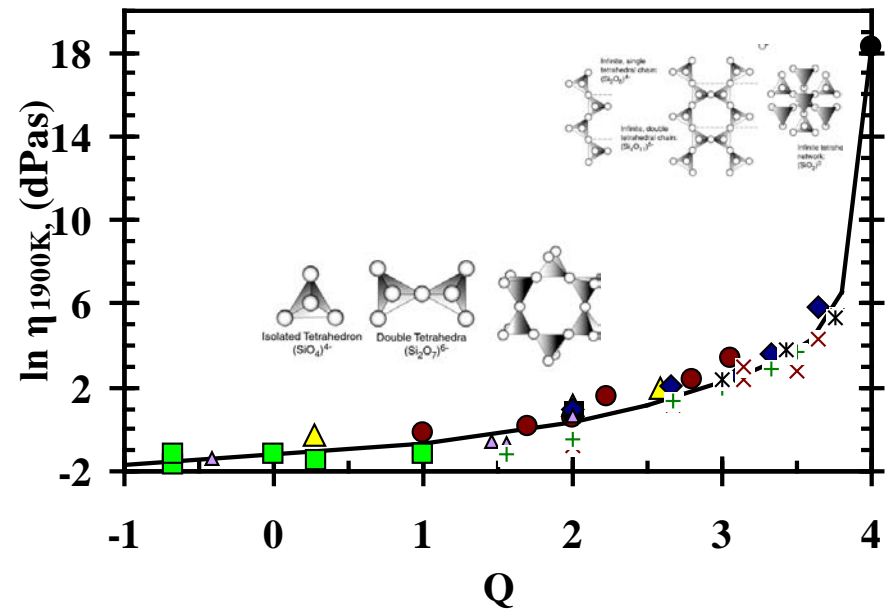
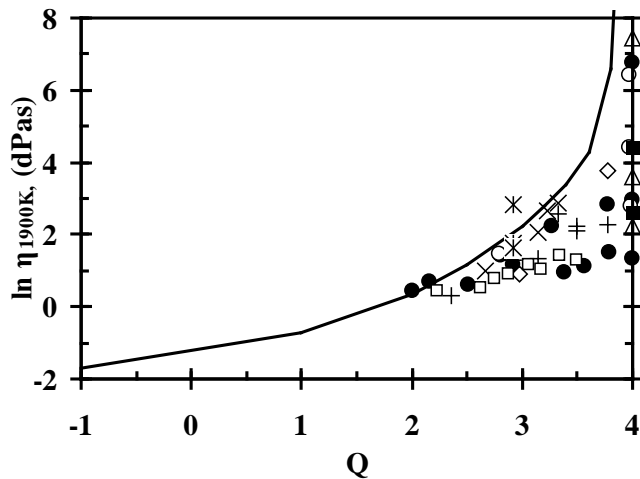
Effect of structure on slag properties

Polymerisation (Q) has great effect on props

$Q \uparrow$ as $\%SiO_2 \uparrow$ as $CaO\% \downarrow$

Alumino-silicates

May be Al-O bond weaker than Si-O bond



Factors affecting properties

Slags- crystals or glasses

Crystals-atoms fixed pos'n

Glasses-disorder- forms

scl- high S_{config} ;

Nature cations \rightarrow structure

Bond strength- (z/ r^2)

$(z/ r^2) \uparrow \rightarrow (Q^n \rightarrow Q^{n-1} + Q^{n+1}) \uparrow$

\rightarrow Coord no $(^{(6)} N) \uparrow$

Size: elect cond. Diffusion

No. (n): Na_2O $n=2$; CaO , $n=1$

Effect of structure- props

1. Viscosity(η) El cond (κ) / Res(R) Diff coeff(D)

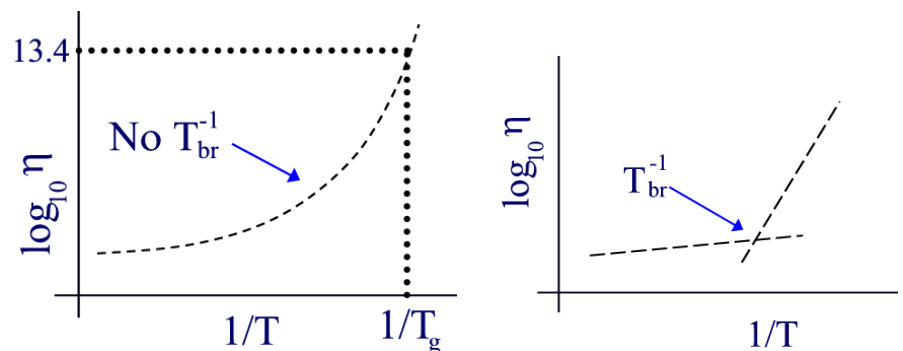
Liq: $\eta = A_A \exp(B_A/T)$

Scl: $\eta = A_V \exp(B_V/(T-T^0))$

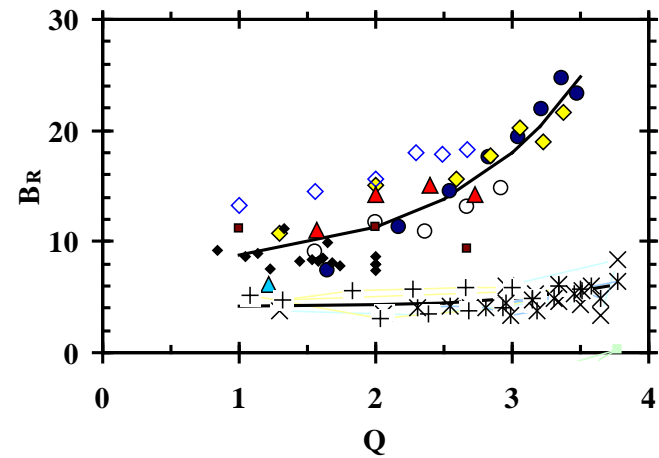
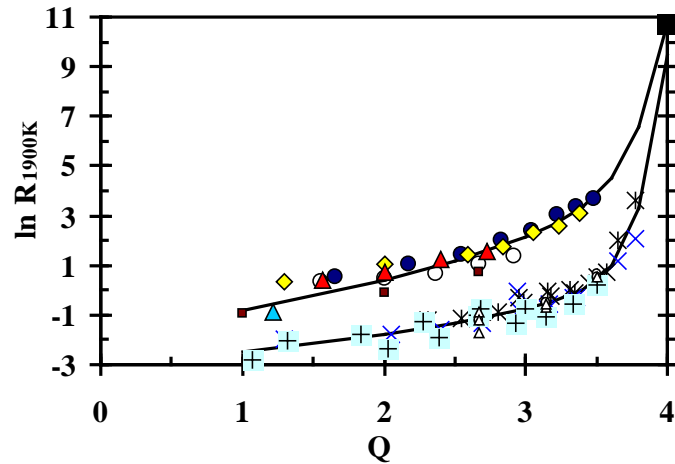
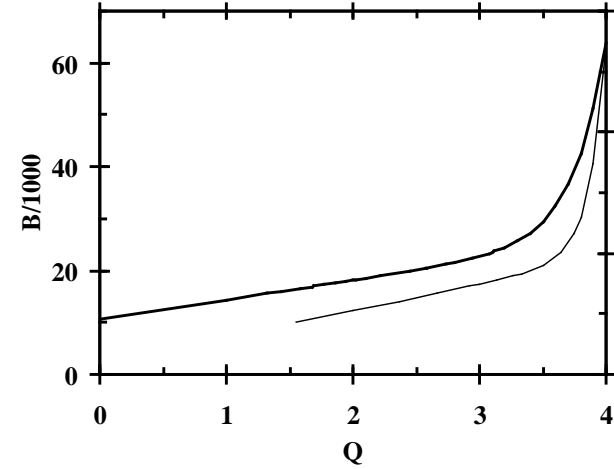
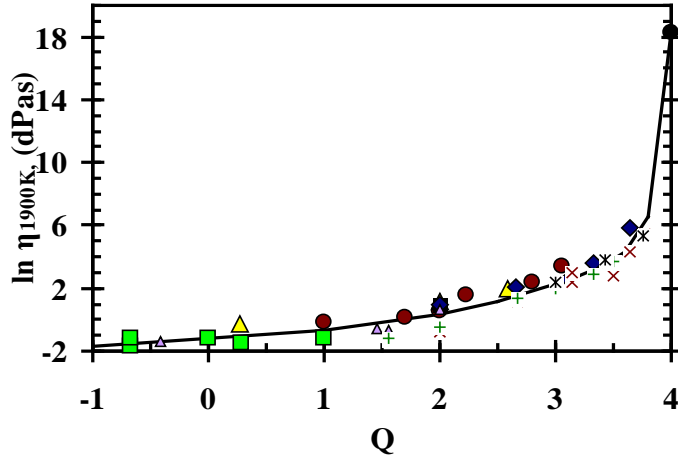
1. Resistance cation movement

2. Mobility of cations size

Equivalent: η ; R; $(1/D)$

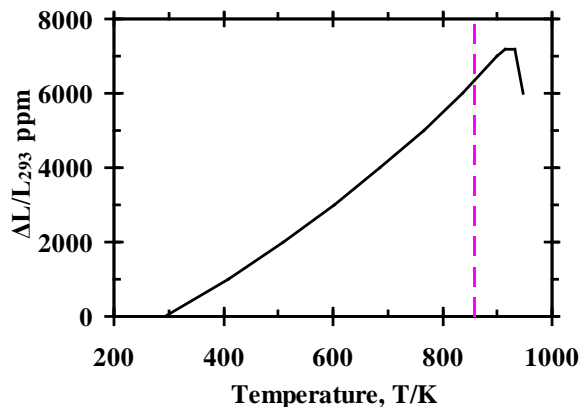


$\ln \eta_{1900K}$; $\ln R_{1900K}$; B_η ; B_R as f (Q)



Density (ρ), Thermal expansion coeff (α, β) Surface and Interfacial tension ($\gamma_{sl}, \gamma_{msl}$)

- $\alpha \uparrow$ as $Q \downarrow$ and $(z/r^2) \downarrow$
 - $\alpha_{\text{glass}} \uparrow$ sharply at T_g -
 - glass \rightarrow scl:
 - $T_g - T_{\text{liq}}$: $\alpha_{\text{scl}} \approx 3 \alpha_{\text{crys}}$
- ρ slightly affected by structure
 $\rho_{\text{crys}} > \rho_{\text{glass}}$ - better packing



$\gamma_{sl}, \gamma_{msl}$ **surface** not **bulk** property

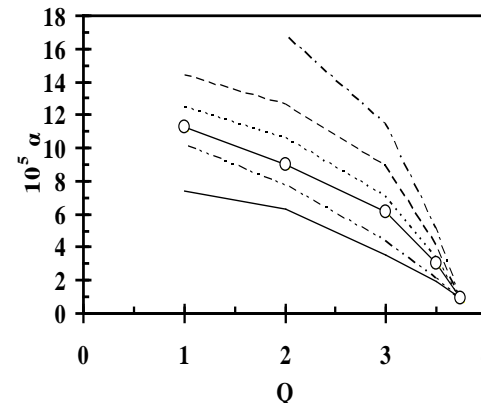
Surfactants- in surface layer
eg. S, O in steel

slags, $B_2O_3, CaF_2, K_2O, Na_2O$

$$\gamma_{msl} = \gamma_m + \gamma_{sl} - 2\phi(\gamma_m \gamma_{sl})^{0.5}$$

$\gamma_m \approx 4 \gamma_{sl}$: γ_m most important

- S, O contents in metal



Thermal conductivity (k) thermal diffusivity (a)

Heat transfer over slag film

-complex-**cond'n**, **rad'n**, **conv**

Solid: $k_{\text{eff}} = k_{\text{lat}} + k_{\text{R}}$

$k_{\text{R}} = 16\sigma n^2 T^3 / 3\alpha^*$

liq glass: $k_{\text{R}} = 10k_{\text{lat}}$

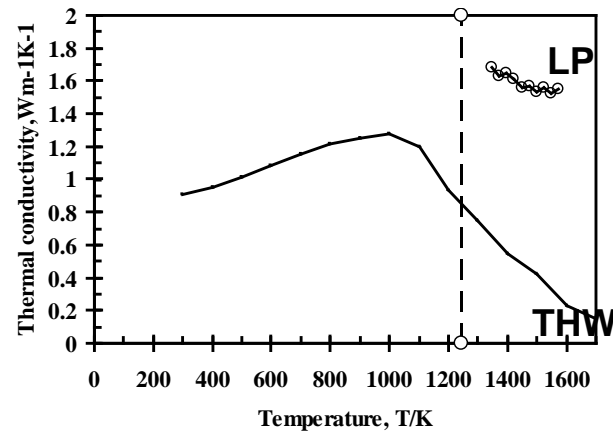
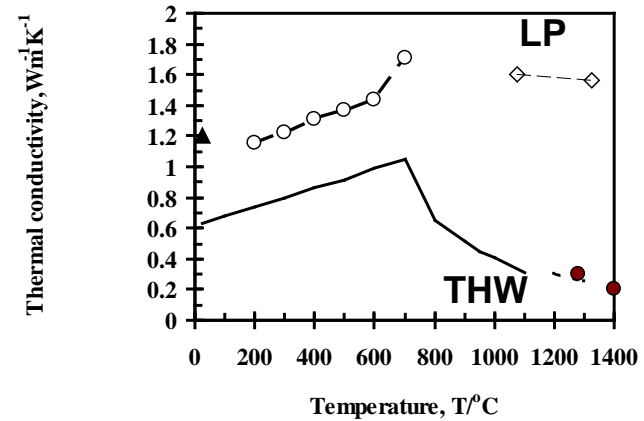
$k_{\text{R}} \downarrow$ by (i) **FeO add'n** (ii) **cryst**

$k_{\text{crys}} \approx 2k_{\text{glass}}$

2 methods: LP and THW

$k_{\text{LP}} \approx 5-10 k_{\text{THW}}$

Problem un-resolved



Manipulation of properties for process optimisation-liquidus temp (T_{liq})

1. Liquidus temp (T_{liq})

Freeze linings- slag attack of refractory – Lurgi

-Slag coating of refractory

Slag splashing- BOS-LD

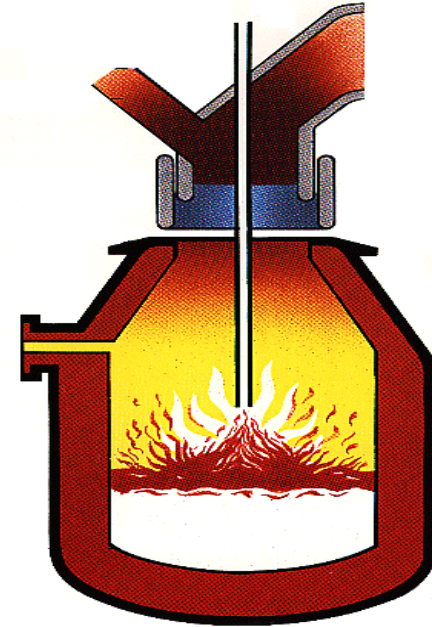
Pig $Fe + O_2 \rightarrow FeO$; $Si \rightarrow SiO_2$

CaO added \rightarrow slag

Great turbulence \rightarrow

Extend refr life and minimise “downtime”

Optim. slag: 13%FeO:8%MgO



Forms $MgO \cdot Fe_2O_3$ - high mp- >50,000 heats without re-lining

Manipulation of slag T_{liq} , viscosity(η)

Drainage rate- ($1/\eta$)

Coal gasification

ash $\rightarrow \uparrow \eta$ slag

CaO added $\rightarrow \downarrow \eta$

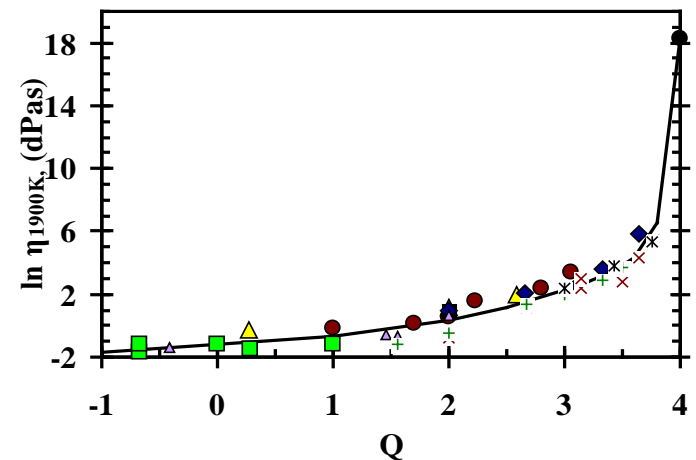
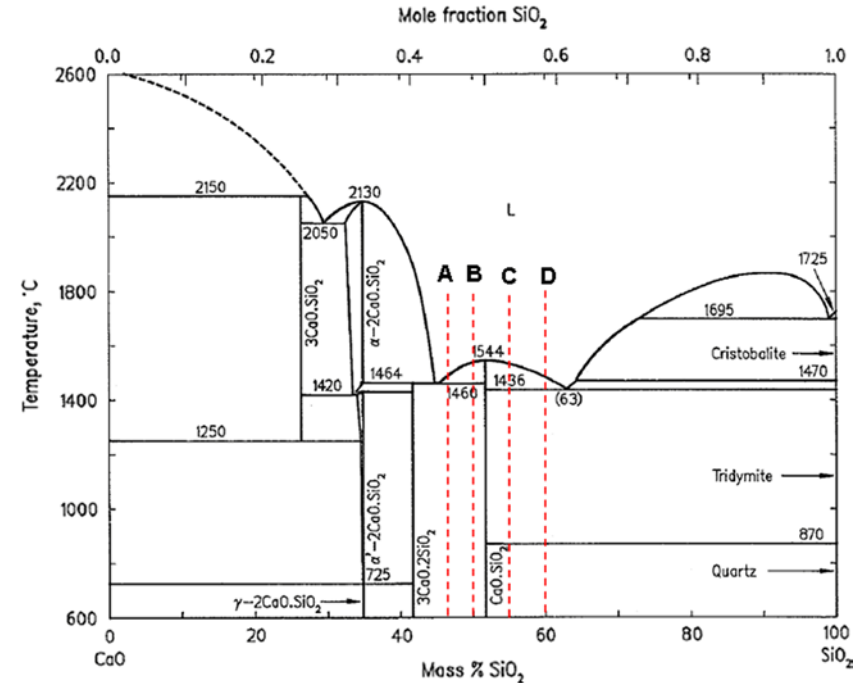
Low melting regions

CaO- SiO_2 : $X_{CaO} = 0.4-0.6$

CaO- Al_2O_3 : $X_{CaO} = (0.5-0.7)$

Fixed amount CaO-
disasters

Ladle glazes \rightarrow inclusions



Manipulation of surface (γ_{sl}) and interfacial tension (γ_{msl})

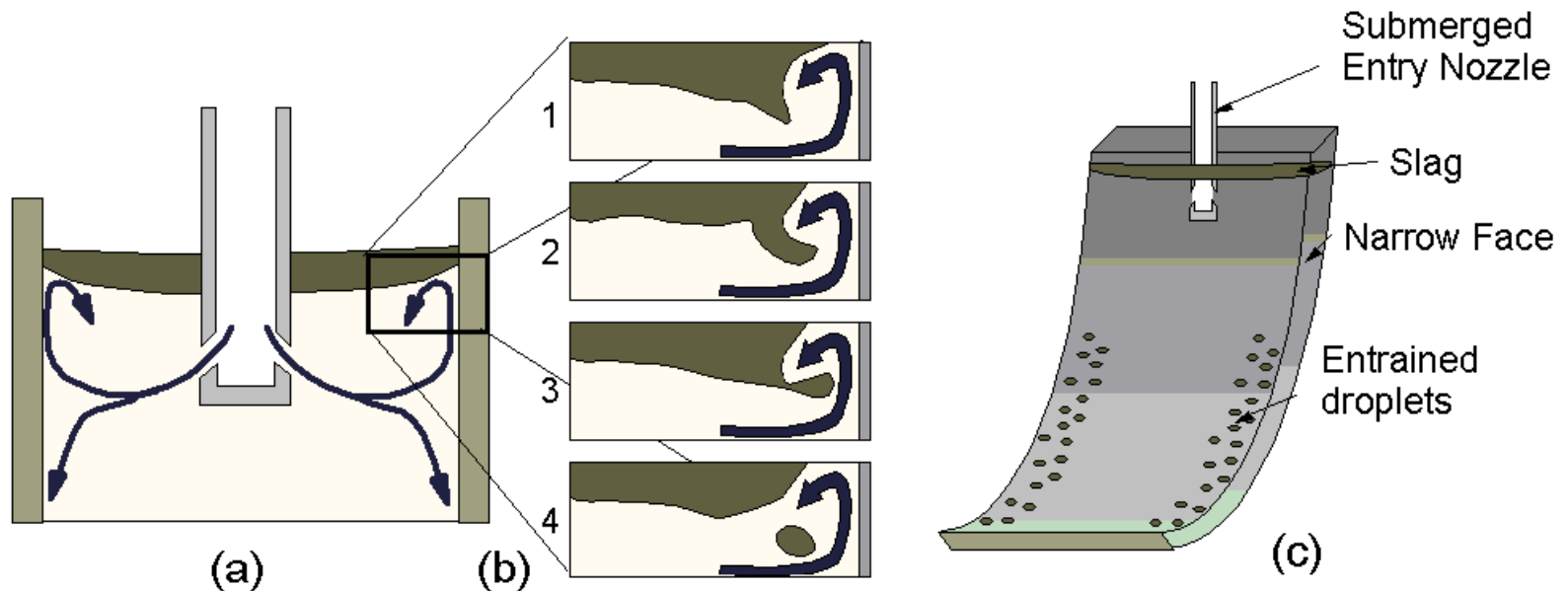
Slag & metal entrainment

- Loss of precious metals
- Inclusions in CC steel

Velocity_{metal} > Velocity_{slag}

$$m_{\text{entrap}} = 1.06 \times 10^{-7} (\eta_{sl})^{-0.255} \cdot (\gamma_{msl})^{-2.18}$$

Min by incr η_{sl} and γ_{msl}



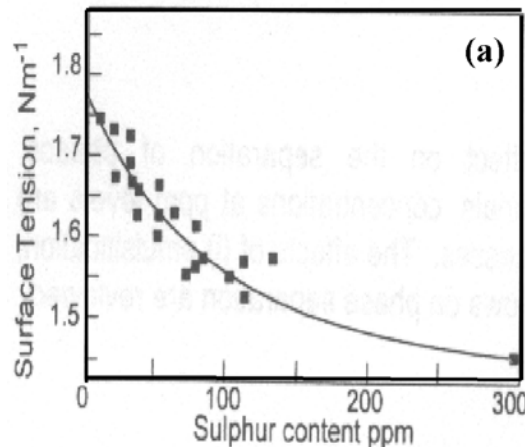
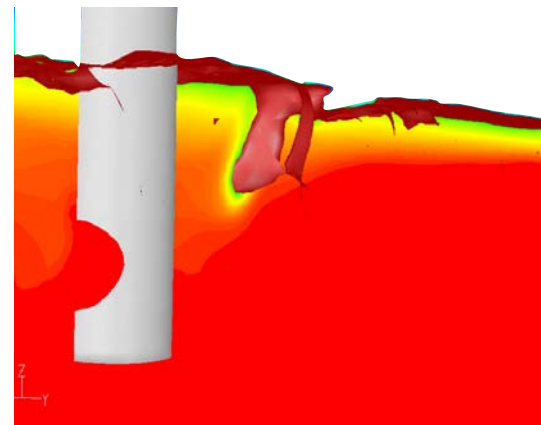
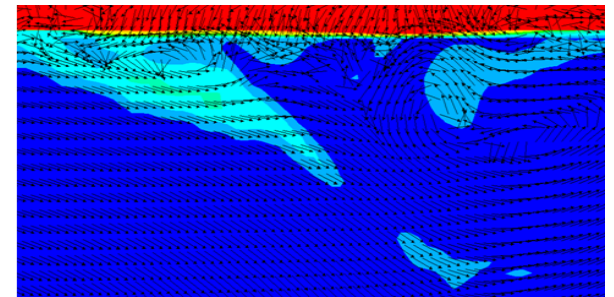
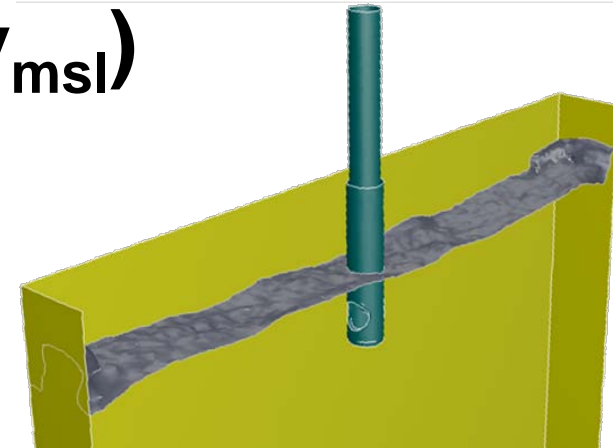
Manipulation of surface (γ_{sl}) and interfacial tension (γ_{msl})

Math Model of CC process

Predicts standing wave
,vortices, “*necking and detachment*”

$$\gamma_{msl} = \gamma_m + \gamma_{sl} - 2\phi(\gamma_m \gamma_{sl})^{0.5}$$

$\gamma_{msl} \uparrow$ as S, O in metal \downarrow
 $B_2O_3, K_2O, Na_2O \downarrow$



Other problems involving surface and interfacial tension

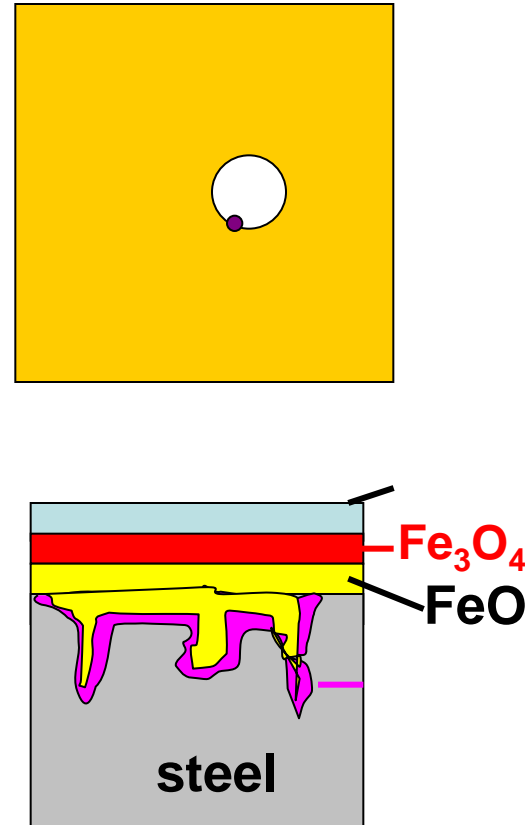
1. Removal of inclusions

By Ar bubbling

2. Scale formation

Na₂O, K₂O cause slag to stick to metal-reacts with FeO → FeSiO₃ (scale)

3. Separation of metal droplets



Manipulation of heat transfer via freeze lining

Heat transfer-very complex

Cracking and stickers

Heat flux, $q - d_s, k_R,$

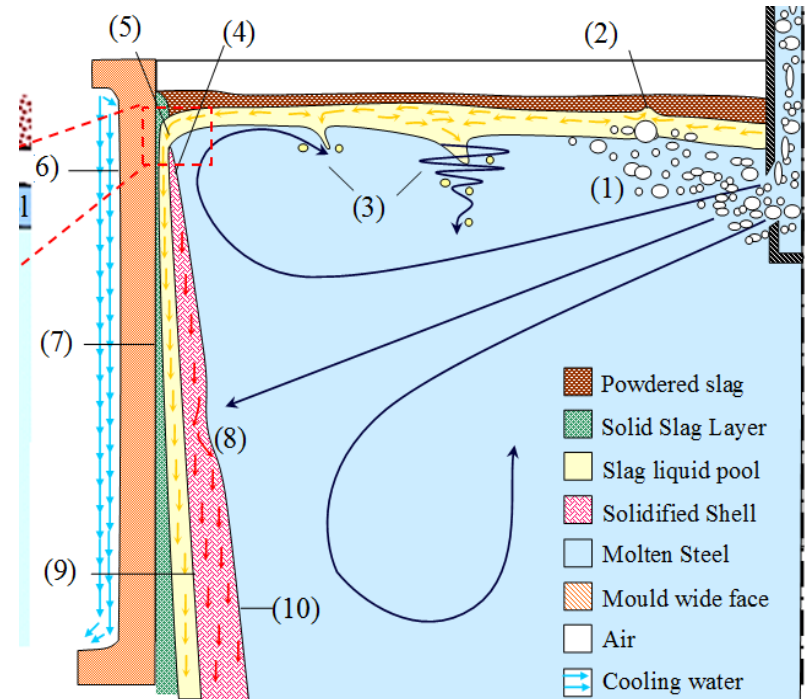
$k_{\text{cryst}} \approx 2k_{\text{glass}} ; q_{\text{cryst}} < q_{\text{glass}}$

Cryst $\uparrow \rightarrow k_R \downarrow$

Heat flux manipulated by

1. $d_s \rightarrow T_{\text{sol}} ; d_s \uparrow \text{ as } T_{\text{sol}} \uparrow$

2. % crystals in slag film



Harvesting enthalpy in slag

Steelmaking

Energy ca. 30% total costs

BOS slag –granulated –
water spray on molten
slag → flame

H₂- decomposition of H₂O

Harvest H₂.

Problem – O₂ + H₂ mixture

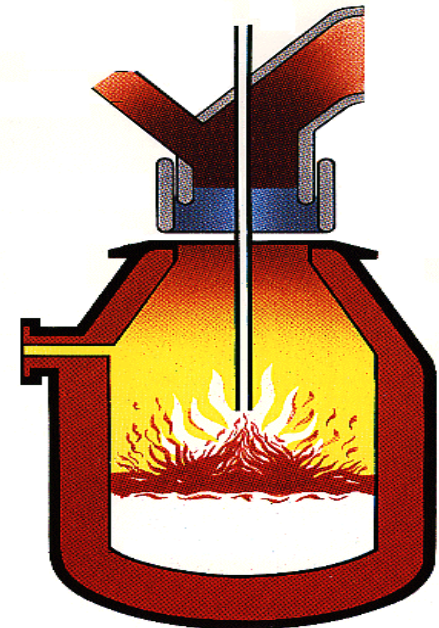
Tata- reseach programme-
estimated saving- 30
million \$ p.a for average
steelworks

Produced

>70% H₂+N₂+CO₂

H₂ could be used for
energy or as reductant

Pilot –ferrochrome plant



Discussion

- Vast range slag compositions high temp processes
- Compositions may change on daily basis
- Need for models to calculate props from chem comp.
- Models should include structural characteristics
- Can represent structure in terms of BO, NBO or Q or thermodynamic functions
- Challenge will be in representing certain structural features eg. Ti^{4+} prefers company of other Ti^{4+} to Si^{4+}

Conclusions

1. **Slag properties proved very useful for solving process problems**
2. **Mathematical models can give insights into mechanisms and help solve problems.**
3. **Knowledge of factors affecting physical properties allows one to manipulate processes- including valorisation**
4. **Vast range of slag compositions in pyro-metallurgy - will need good models to estimate properties from chemical comp'n- where structure comes in.**